

Fig. 1 Conical shell with a transverse element under strain.

The results were based upon height and volume changes,  $dh$  and  $dv$ , associated with a transverse element of the tank of infinitesimal height  $h$ . In the limit  $h \rightarrow dL$ . However, it has been found that the integrals of these quantities do not, in general, add up to the correct expressions for the total changes in tank height and volume, respectively. Instead, one should use alternative quantities  $dh_E$  and  $dv_E$ , which represent the height and volume increases effectively contributed to the over-all tank. Expressions for  $dh_E$  and  $dv_E$  are derived herewith. They can be substituted directly for  $dh$  and  $dv$  as used in Ref. 1. For a cylindrical tank, for which the cone angle  $\phi = 0$ , the expressions become identical. For small values of  $\phi$  the error is negligible. In fact, for the numerical results presented in Fig. 6 of Ref. 1 the largest error in calculation is less than 0.05%. Thus, the conclusions of Ref. 1 are not changed.

### Discussion

Consider a cone frustum, the cross-sectional view of which is represented by  $pqrs$  in Fig. 1. An element of infinitesimal height  $h$ , which in the limit becomes  $dL$ , is represented by  $abcd$ . The shell is of infinitesimal thickness  $T$ , so that membrane theory is applicable to its behavior under strain (no stress can be developed perpendicular to the tangent plane at any point on the shell, and no bending moment can be set up). Strain in the element  $abcd$  produces small deflections as follows:

1) Due to circumferential strain  $\epsilon_\theta$ , the element  $abcd$  expands and deflects to configuration  $efg'h'$ , where  $g'h' = cd(1 + \epsilon_\theta)$ , and  $ef = ab(1 + \epsilon_\theta)$ , while  $eh'$  remains equal to  $ad$ .

2) Due to meridional strain  $\epsilon_\phi$ , the element  $efg'h'$  stretches and deflects into the configuration  $efgh$  where  $eh = eh'(1 + \epsilon_\phi)$ , while  $gh$  remains equal to  $g'h'$ .

Thus, the volume of the element increases by an actual amount  $dv$  to become the volume represented by  $efgh$ . However, the volume of the frustum  $pqrs$  increases by an effective amount  $dv_E$  to become equal to that represented by  $pqbfgmtunheap$ . The volume represented by  $cdsr$  translates as a rigid body into position  $mnut$  without change. The effective volume increment  $dv_E$  is, therefore, equal to the volume of a solid obtained by rotating the shaded area  $cbfgmneadc$  about the cone's axis of symmetry. The quantities  $dv_E$  and  $dh$  are not equal. In Ref. 1  $dv$  and  $dh$  were used by mistake for integration between limits to obtain expressions for the total volume and height increases, respectively, of a conical

frustum. The correct procedure is to integrate  $dv_E$  and  $dh_E$  instead.

Using the same nomenclature as Ref. 1—i.e.,  $n_\theta$  and  $n_\phi$  are circumferential and meridional running skin loads, respectively—the expressions for  $dh_E$  and  $dv_E$  can be written as follows:

$$dh_E = (1/T \cos^2 \phi)(n_\phi/E_{Mh} - n_\theta/E_{Hh})dL \quad (1)$$

$$dv_E = (\pi r^2/T \cos^2 \phi)(n_\phi/E_{Mv} + n_\theta/E_{Hv})dL \quad (2)$$

where  $E_{Mh} = E_\phi$ ,  $E_{Hh} = E_\theta/\nu_{\phi\theta}$ ,  $E_{Mv} = E_\phi/(1 - 2\nu_{\phi\phi})$ , and  $E_{Hv} = E_\theta/(2 - \nu_{\phi\theta})$ ;  $E_\phi$  and  $E_\theta$  are Young's moduli in the two principal directions, and  $\nu_{\phi\theta}$  and  $\nu_{\theta\phi}$  are the Poisson coefficients for anisotropic material.

Equations (1) and (2) herewith are equivalent to Eqs. (3) and (4) of Ref. 1 and may be substituted directly in all subsequent parts of Ref. 1.

On page 14 of Ref. 2 Lekhnitskii states that  $E_\theta\nu_{\theta\phi} = E_\phi\nu_{\phi\theta}$  always. Making use of this theorem, it can be seen that when  $\phi = 0$  the expressions for  $dh$  and  $dv$  as given in Eqs. (3) and (4) of Ref. 1 become identical with those of Eqs. (1) and (2) given herewith for  $dh_E$  and  $dv_E$ . Thus, for small values of  $\phi$  the discrepancy becomes negligible.

### References

- 1 Pengelley, C. D., "Natural Frequency of Longitudinal Modes of Liquid Propellant Space Launch Vehicles," *Journal of Spacecraft and Rockets*, Vol. 5, No. 12, Dec. 1968, pp. 1425-1431.
- 2 Lekhnitskii, S. G., *Theory of Elasticity of an Anisotropic Elastic Body*, Holden-Day, San Francisco, Calif., 1963.

## Erratum: "Orbital Gyrocompassing Heading Reference"

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R. A. CARLSTROM of Huntington, New York was kind enough to point out an error in a figure I prepared. Figure 1 should replace Fig. 4 of the subject paper.

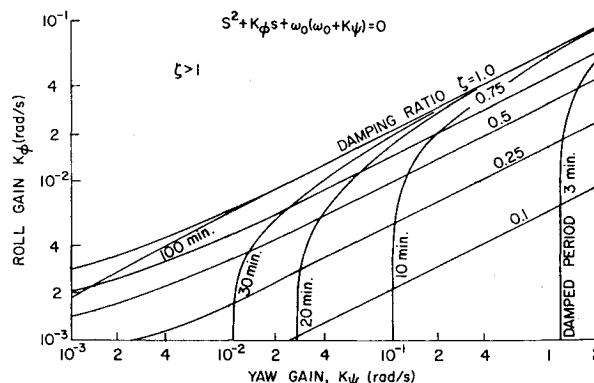


Fig. 1 Natural period and damping of gyro compass as a function of gains in Fig. 3.

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